

Recycle Ponds Initial Inflow Design Flood Control System Plan

Independence Steam Electric Station Newark, Independence County, Arkansas

October 2018

Prepared For Entergy Arkansas, Inc.

R. Kent Nilsson, P.E.

ROFESSIONAL

Senior Engineer

Jason House

Project Manager

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Revision History

Revision Number	Revision Date	Section Revised	Summary of Revisions

Section 1 Background

Entergy Arkansas (Entergy) operates the Independence Steam Electric Station (Plant), located at 555 Point Ferry Rd, Newark, AR 72562. This Plant operates two Water Recycle Ponds: East and West (Ponds), as part of its process water system for bottom ash transport. Pursuant to United States Environmental Protection Agency (USEPA) Disposal of Coal Combustion Residuals (CCR) From Electric Utilities Final Rule (CCR Rule) Section 40 Code of Federal Regulations (CFR) § 257.82, this Initial Inflow Design Flood Control System Plan (Plan) presents the design and construction features of the Ponds that adequately manage and maintain the inflow design flood control system.

1.1 Documents Reviewed

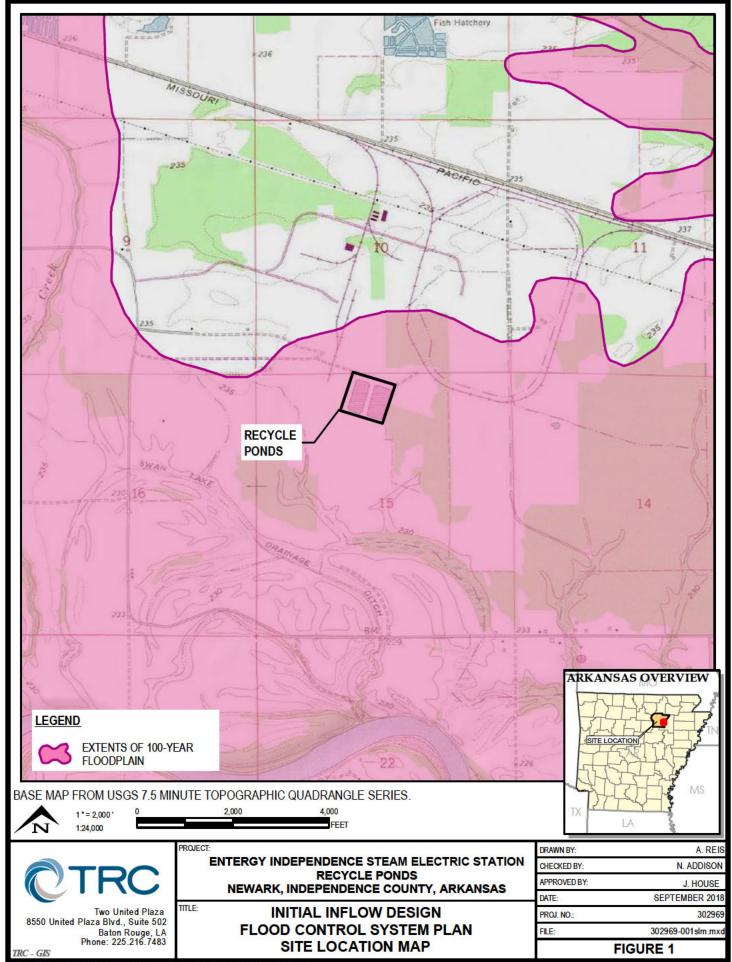
To develop this plan the following documents were reviewed by TRC:

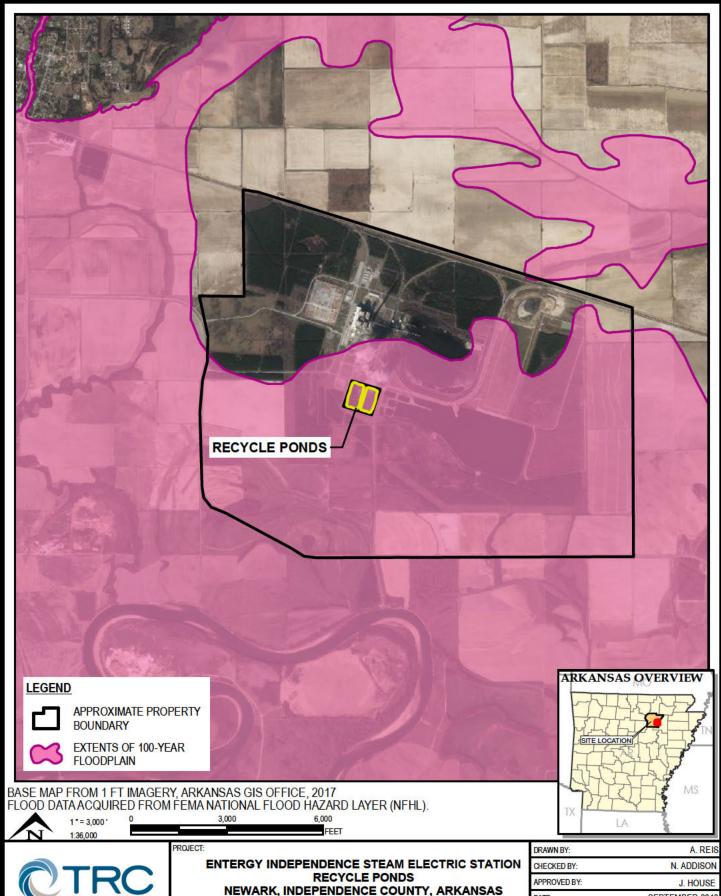
- Entergy's Independence Steam Electric Station Bottom Ash Work Plan. Document SD-1204.05A. Rev 2. November 10, 2008.
- Outfall Locations and Drainage Plan developed by Woodward Clyde Consultants, File No. 92T156C-A106. Rev 1. 8/23/16
- Topographic Survey performed by B&F Engineering, Inc. 10/4/18
 - Recycle Ponds Plan View. Drawing EX 1/2

1.2 Existing Conditions

The Plant is located near Newark, Independence County, Arkansas (Figure 1). The Plant is located at approximate latitude 35°40′39″ N, longitude 91°24′42″ W (front gate). The Ponds are located on the southern side of the Plant. The East and West Ponds have an approximate surface area of 7.0 acres each. The typical water level elevation in each pond is approximately 235 ft North American Vertical Datum of 1988 (NAVD88) based on field observations during July 2018. Topography surrounding the immediate vicinity of the Ponds is generally flat-lying, with existing ground surface elevations ranging from approximately 235 to 239 ft NAVD88. Natural topography in the vicinity of the ponds is relatively flat to gently sloping.

Water contained in the Ponds is part of the facility's bottom ash transport system. There are storm water swales around the Ponds to control storm water and limit the volume of run-on. The natural ground beyond the ponds gently slopes to the southwest. A topographic survey completed by B&F Engineering, Inc. in October 2018(b) confirmed the elevations of the top of ground surface surrounding the ponds and the other surrounding areas.







8550 United Plaza Blvd., Suite 502 Baton Rouge, LA Phone: 225.216.7483 **NEWARK, INDEPENDENCE COUNTY, ARKANSAS**

INITIAL INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN SITE DETAIL

FI	GURE 2
FILE:	302969-002.mxd
PROJ. NO.:	302969
DATE:	SEPTEMBER 2018
APPROVED BY:	J. HOUSE
CHECKED BY:	N. ADDISON
DRAWN BY:	A. REIS

TITLE:

Section 2 Inflow Design Flood Control

40 C.F.R. § 257.82 specifies requirements for hydrologic and hydraulic capacity of CCR units. The purpose of this report is to demonstrate the hydrologic and hydraulic capacity of the Ponds meet the requirement of the CCR Rule. Per ERM's Report, the Ponds are incised, therefore, a hazard potential classification is not needed per 40 CFR § 57.73(a). Based on the incised potential classification, the CCR surface impoundment unit must adequately manage flow into the unit during and following the peak discharge of the 25-year flood (40 CFR 257.82(a)(3)(iv)).

The Ponds were designed and utilized as part of the Plant's bottom ash transport water system. The design meets the requirements of 40 CFR § 257.82(a)(1), (2) and (3), which states:

- (1) The inflow design flood control system must adequately manage flow into the CCR unit during and following the peak discharge of the inflow design flood specified in paragraph (a)(3) of this section.
- (2) The inflow design flood control system must adequately manage flow from the CCR unit to collect and control the peak discharge resulting from the inflow design flood specified in paragraph (a)(3) of this section.
- (3) The inflow design flood is:
- (i) For a high hazard potential CCR surface impoundment, as determined under § 257.73(a)(2) or §257.74(a)(2), the probable maximum flood;
- (ii) For a significant hazard potential CCR surface impoundment, as determined under 257.73(a)(2) or §257.74(a)(2), the 1000-year flood;
- (iii) For a low hazard potential CCR surface impoundment, as determined under 257.73(a)(2) or §257.74(a)(2), the 100-year flood;
 - (iv) For an incised CCR surface impoundment, the 25-year flood.

The Flood Insurance Rate Map (Federal Emergency Management Agency, 2010) indicates that the Ponds are located in an area mapped in Zone A of the special flood hazard areas subject to inundation by the 1 percent annual chance flood, refer to Appendix A. Figures 1 and 2 show the extents of the 100-year flood plain. Zone A is an area on the Flood Insurance Rate Map where the base flood elevation has not been determined. Therefore, to estimate the elevation of the 25-year flood for this Plan, an interpolation was performed using the nearest upstream and

downstream locations where the flood elevations had been determined in the Flood Insurance Study (Federal Emergency Management Agency, 2012). This estimate resulted in a 25-year flood elevation of approximately elevation 235 in the vicinity of the Ponds. Based on this result and the survey information, the Ponds are assumed to be above the elevation of the 25-year flood; therefore, a dedicated system to control flood waters is not required. The Ponds have been designed with inflow features presented in the sections below to mitigate and control stormwater inflows during a 25-year storm event.

In addition to the flood control requirements above, 40 C.F.R § 257.82(b) addresses discharges:

Discharge from the CCR unit must be handled in accordance with the surface water requirements under §257.3-3.

The Ponds were designed and utilized as part of the Plant's bottom ash transport water system and comply with the requirements of 40 CFR § 257.82(b). Water discharges from the Plant are permitted through the Arkansas Department of Environmental Quality (ADEQ) for the National Pollutant Discharge Elimination System.

2.1 Recycle Ponds Operation

The Ponds are utilized as part of the Plant's bottom ash transport water system. Site infrastructure enables the Ponds to be operated either singularly, in parallel, or in series. The Ponds can be drained via pumps in a pump house located between the ponds with a 30-inch intake pipe from each pond. The Ponds were designed to operate with 2 feet of freeboard, height difference from the top of the surrounding ground surface to the design water level. In the event both Ponds reach capacity, overflow from the Ponds flows through a culvert and ditch located in the north west corner of Pond A. The ditch discharges to the surge pond.

The following control measures are implemented during operation to control the water levels in the Ponds:

- Operate pumps as needed to control the pond water levels.
- Regularly check and maintain grades surrounding the ponds to minimize the area contributing to storm water run-on.

2.2 Run-on Control

As designed, the Ponds meet the requirement to control the storm water run-on from a 25-year, 24-hour storm event based upon the Precipitation Frequency Estimates from the National Oceanic and Atmospheric Administration. As designed, the Ponds meet the requirement to operate with at least two feet of freeboard. The storm water run-on volume calculated for the

design storm was compared to the storage capacity above the Ponds design operating elevation. The evaluation determined that there is sufficient capacity in the Ponds when operating with two feet of freeboard to accept run-on volume from a 25-year, 24-hour storm event, refer to Appendix B.

2.3 Pumping Capacity

The pump station is equipped with six (three per unit) Gould single stage centrifugal pumps with a rated pumping capacity of 2750 gallons per minute (gpm) at 307 feet of head in the LP Ash Water Pump house. A calculation was performed to determine length of time required to remove the anticipated run-on due to a 25-year, 24-hour storm event, refer to Appendix B. The calculation was performed assuming only two operational pumps and resulted in a required time of 10.3 hours or approximately .5 days to remove the anticipated storm water run-on collected in both Ponds. This calculation shows that pumping rates are sufficient in controlling water levels in the Ponds.

2.4 Conclusions

The Ponds meet the requirements of 40 CFR § 257.82 of adequately controlling the inflows and outflows of peak discharge at the Plant for the following reasons:

- The Ponds are located above the 25-year flood elevation.
- The Ponds were adequately designed to withstand a 25-year, 24-hour storm event.
- The pumping rates are sufficient to control the water levels in the Ponds.

Section 3 Notifications

In accordance with 40 CFR § 257.105(g), Entergy will post to the Plant's Facility Operating Record (FOR) the Initial Inflow Design Flood Control System Plan. The Director of the ADEQ will be notified when documents are available as per 40 CFR § 257.106(g) and notices and documents will be placed on Entergy's CCR website consistent with 40 CFR § 257.107(g).

Section 4 Amendment and Periodic Plan Revision

In accordance with 40 CFR § 257.82(c)(2), Entergy may amend this Initial Inflow Design Flood Control System Plan at any time. Specifically, Entergy will amend the inflow design flood control system plan whenever there is a change in the operation of the CCR unit that would substantially affect the written plan in effect. A periodic inflow design flood control system plan must also be prepared every 5 years from the completion date of this plan. Recordkeeping, Notification and Posting requirements of 40 CFR § 257.105, 257.106 and 257.107 will be followed.

Section 5 References

- B&F Engineering, Inc. 2018b. Topographic Survey: Independence Recycle Ponds Entergy Arkansas. October 4, 2018. Drawing.
- Federal Emergency Management Agency. 2012. Flood Insurance Study: Independence County, Arkansas and Incorporated Areas. Flood Insurance Study Number 05063CV000B. Revised March 15, 2012. United States Department of Homeland Security. Washington, D. C.
- Federal Emergency Management Agency. 2010. Flood Insurance Rate Map: Independence County, Arkansas and Incorporated Areas. Panel 400 of 550. Map Number 05063C0400D. Effective Date March 17, 2010. National Flood Insurance Program. Washington, D. C.
- ERM. 2018b. Summary of Site Visit and Review of CCR Structural Integrity Criteria Requirements for Entergy Independence Steam Electric Station (ISES) Recycle Pond. October 2018.

Section 6 Certification

I, the undersigned Arkansas Professional Engineer, hereby certify that I am familiar with the technical requirements of 40 CFR § 257.82. I also certify that it is my professional opinion that, to the best of my knowledge, information, and belief, that the information in this inflow design flood control system plan is in accordance with current good and accepted engineering practice(s) and standard(s) and meets the technical requirements of 40 CFR § 257.82(c).

For the purpose of this document, "certify" and "certification" shall be interpreted and construed to be a "statement of professional opinion." The certification is understood and intended to be an expression of my professional opinion as an Arkansas Licensed Professional Engineer, based upon knowledge, information, and belief. The statement(s) of professional opinion are not and shall not be interpreted or construed to be a guarantee or a warranty of the analysis herein.

R. Kent Nilsson

Printed Name of Professional Engineer

State of Arkansas License Number

10/24/18

Signature of Professional Engineer

Date

Appendix A Flood Information

- Flood Insurance Rate Map
- 25-Year Flood Elevation Estimate

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program, It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult her Flood Profiles and Floodway Data and/or Summany of Stillwater Elevations tables contained within the Flood insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.07 North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplan management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood insurance Program. Floodway widths and other perinent floodway data are provided in the Flood insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures.**Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance for this jurisdiction.

Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Arkansas State Plane north zone (FIPSZONE 0301). The horizontal datum was NAD83, GRS1980 spheroid. Differences in datum, spheroid, projection or State Plane zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of the FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1989, visit he National Geodetic Survey website at http://www.ngs.neas.gov/ or contact the National Geodetic Survey website at http://www.ngs.neas.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, NNGS12 National Geodetic Survey SSMC- 3, #8202 1315 East- West Highway Silver Spring, MD 20910- 3282

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at http://www.nos.noag.og/u.

Base map information shown on the FIRM was provided in digital format by the Arkansas Geographic Information Office, 2007.

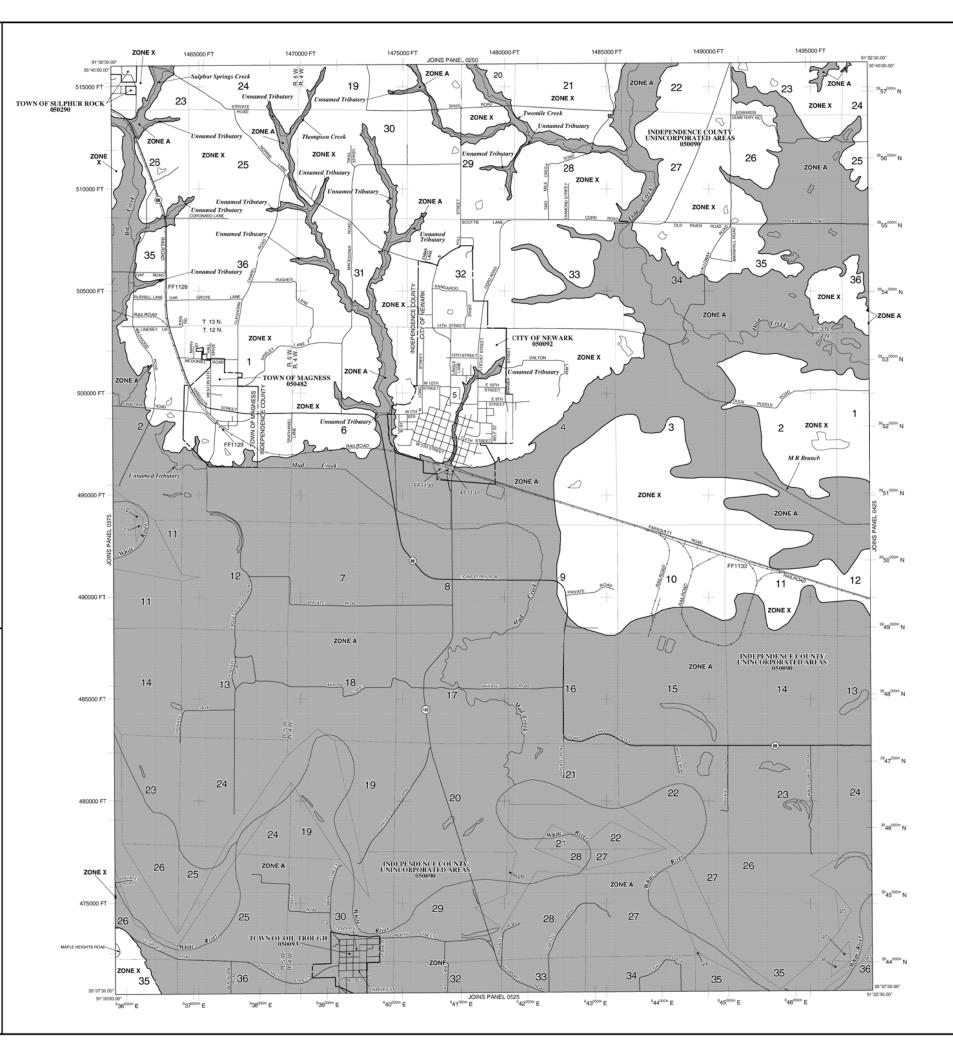
This map reflects more detailed and up-to-date stream channel configurations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study report (which contains authoritative hydractic data may reflect stream channel concess that office from what is shown on this map.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community cificials to verify current corporate limit locations.

Please refer to the separately printed **Map** Index for an overvew map of the courty showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact the FEMA Map Service Center at 1-800-358-9616 for information or available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Pood Insurance Study report and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-803-358-9620 and its website at http://www.mcs.fema.gov/

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA webste at http://www.fema.gov/.



LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Spocial Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Spocial Flood Hazard include Zones A, AE, AH, AO, AR, ASP, V and VE. The Base Flood Flexator is the water-suffice elevation of the 1% annual chance flood.

ZONE A No Base Flood Elevations determ

ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.

ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities

EAR Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the floremer flood control system is being restored to provide protection from the 1% annual chance or greater flood.

greater flood.

99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood. Floodings

ZONE V Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.

ONE VE Coastal flood zone with velocity hazard (wave action); Base Fi

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroschment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

ZONE X

ONE X Areas determined to be outside the 0.2% annual chance floodplain.

ONE D Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Area

Floodway boundary
Zone D boundary
CBRS and OPA boundary

CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.

Base Flood Elevation line and value; elevation in feet*

(EL 987) Base Flood Elevation value where uniform within zone; elevation in feet*

* Referenced to the North American Vetical Datum of 1988 (NAVD 88)

A Cross section line

(23) Transect line

Transect line

Geographic coordinates referenced to the North Ameri
Dahum of 1983 (MAD 83)

Datum of 1989 (NAD 83)

1000-net 1990 (NAD 83)

1000-n

DX5510 Bench mark (see explanation in Notes to Users section of this FIRM panel)

5 River Mile
MAP REPOSITORIES

EFFECTIVE DATE OF COUNTYWDE FLOOD INSURANCE RATE MAP March 17, 2010 EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

For community map revision history prior to countywide mapping, refer to the Community Map History able located in the Flood Insurance Study report for this jurisdiction.

PROGRAM

PANEL 0400D

FIRM FLOOD INSURANCE RATE MAP

INDEPENDENCE COUNTY, ARKANSAS

AND INCORPORATED AREAS

PANEL 400 OF 550

(SEE MAP INDEX FOR FIRM PANEL LAYOUT;
CONTAINS:
COMMUNITY NUMBER PANEL SUFFIX

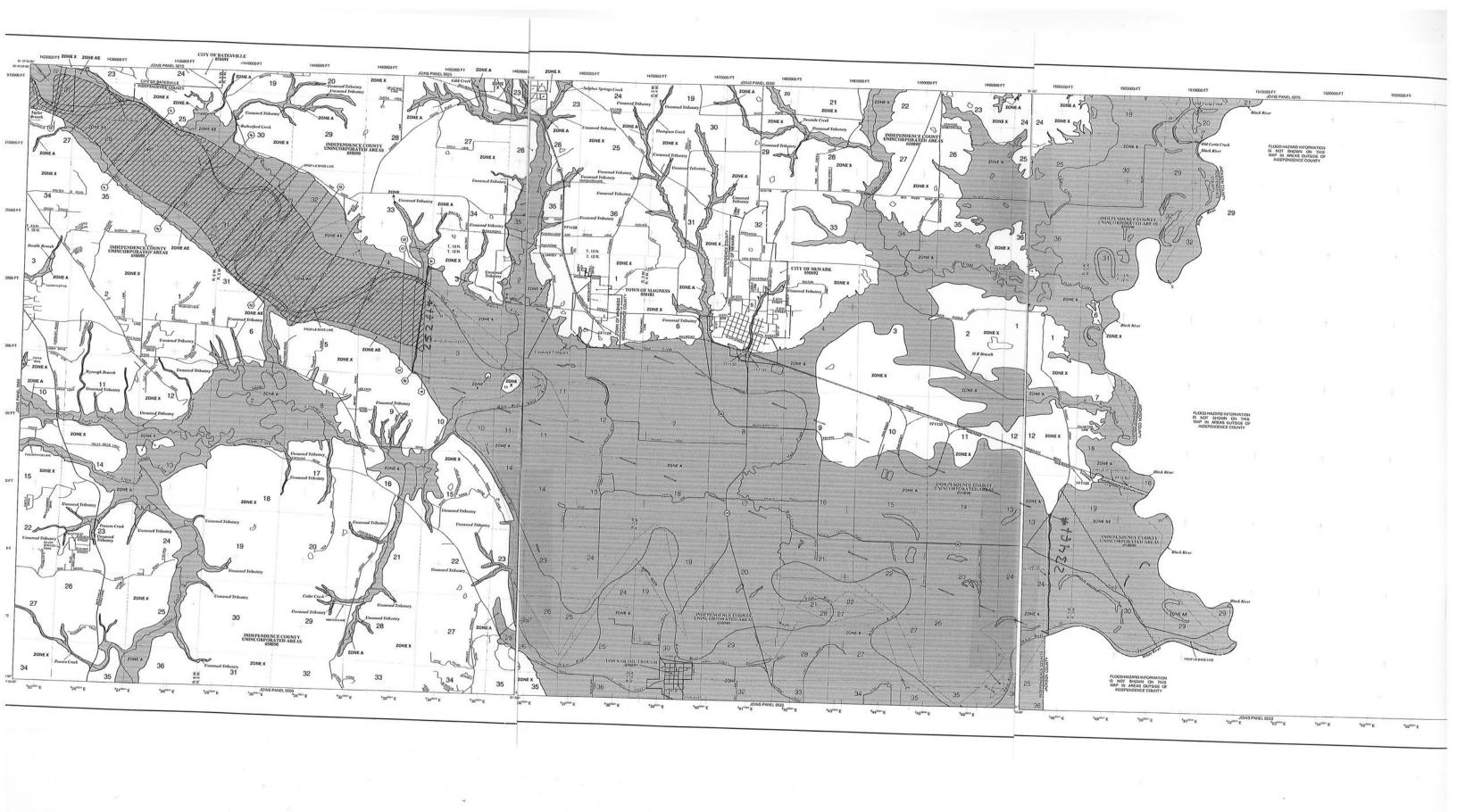
INDEPENDENCE COUNTY 050090 MAGNESS, TOWN OF 050482 NEWARK, CITY OF 050092 OIL TROUGH, TOWN OF 050993 SULPHUR ROCK, TOWN OF 050290

to User: The **Map Number** shown below should be then placing map orders; the **Community Number** show



05063C0400D EFFECTIVE DATE MARCH 17, 2010

Federal Emergency Management Agency





INDEPENDENCE COUNTY, ARKANSAS AND INCORPORATED AREAS

Community Name	Community Number
BATESVILLE, CITY OF	050091
CAVE CITY, CITY OF	050313
CUSHMAN, TOWN OF	050403
MAGNESS, TOWN OF	050482
MOOREFIELD, TOWN OF	050483
NEWARK, CITY OF	050092
OIL TROUGH, TOWN OF	050093
PLEASANT PLAINS, TOWN OF	050484
SULPHUR ROCK, TOWN OF	050290
INDEPENDENCE COUNTY (UNINCORPORATED AREAS)	050090

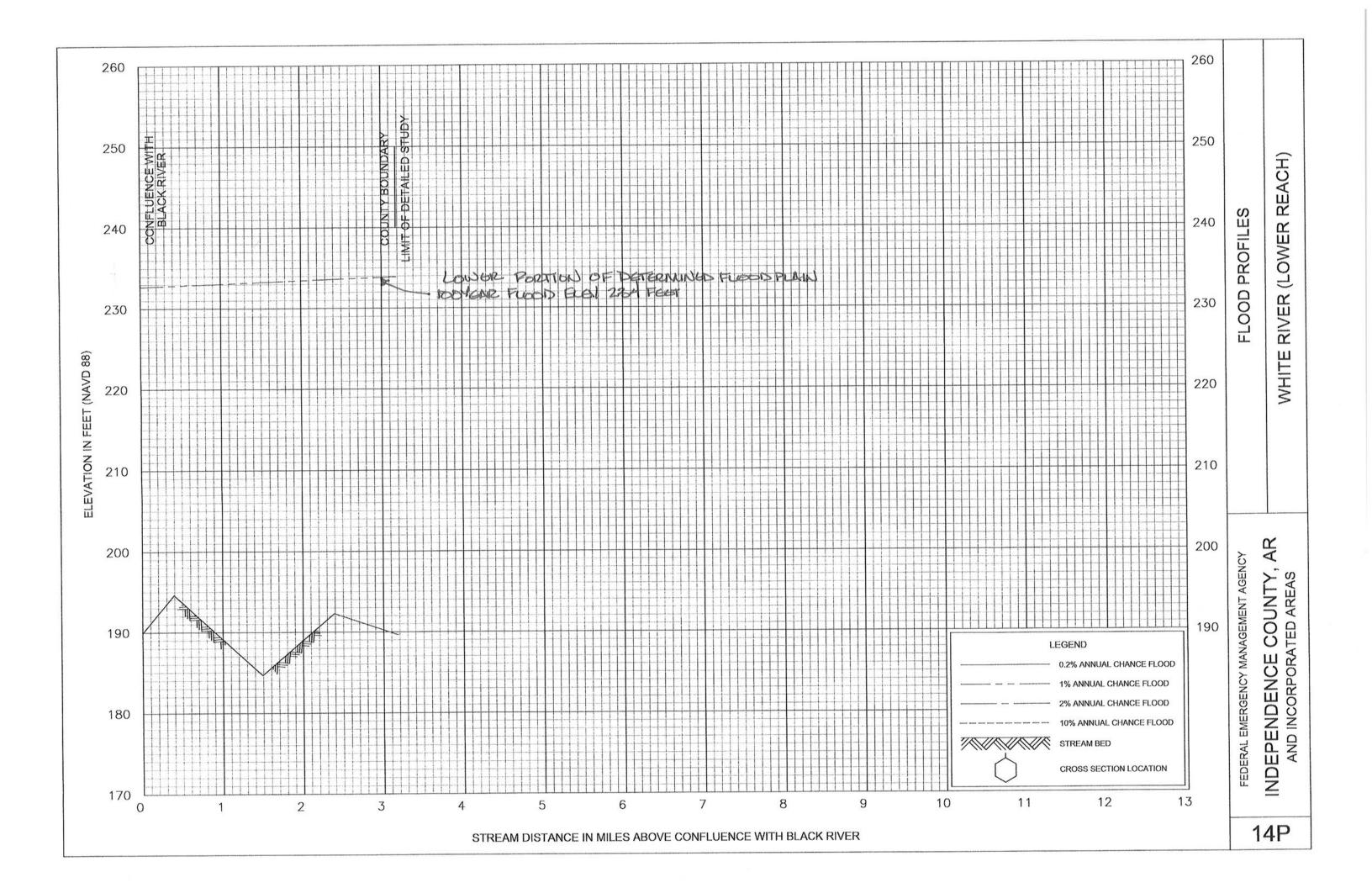


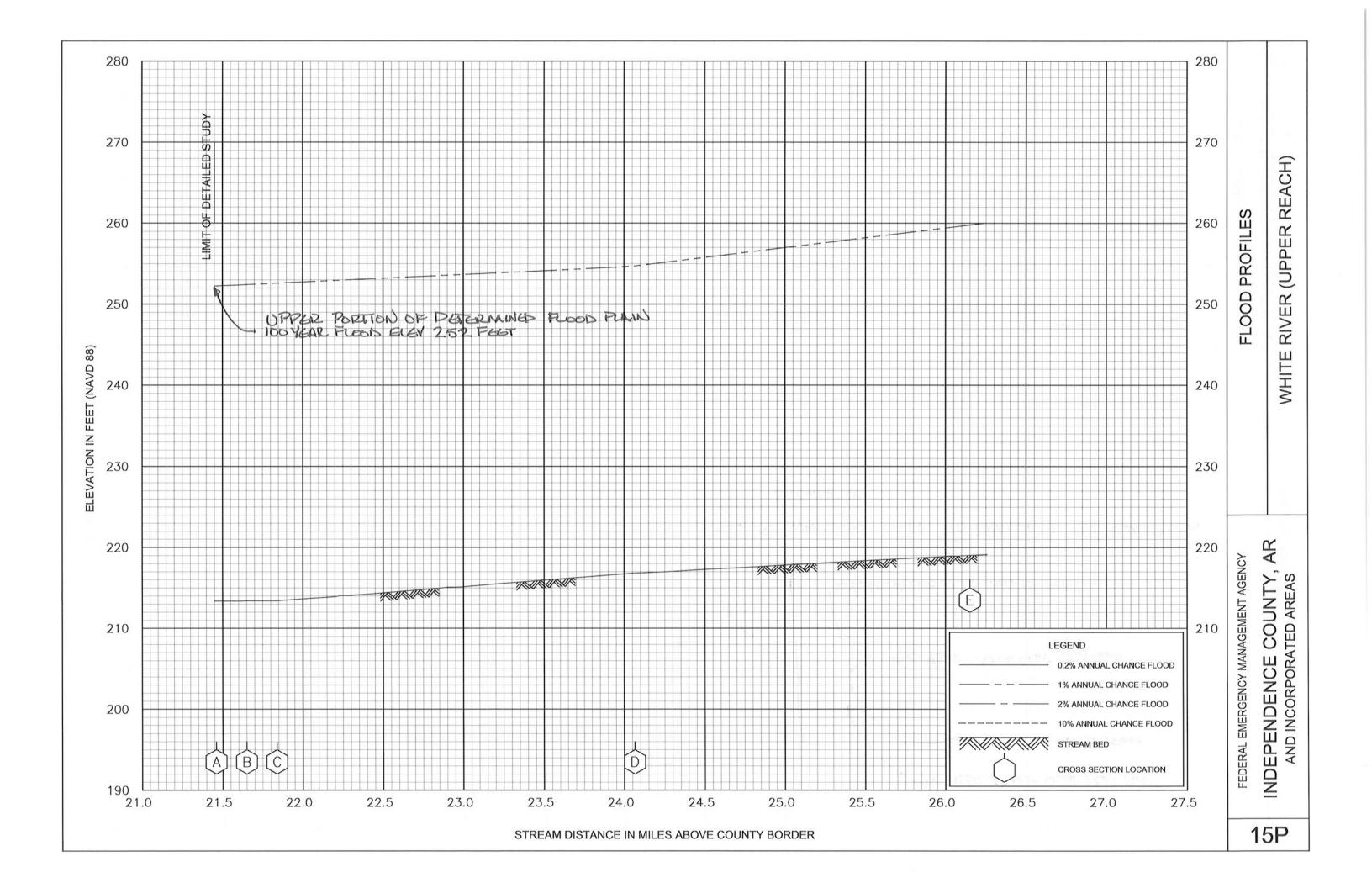
REVISED: March 15, 2012

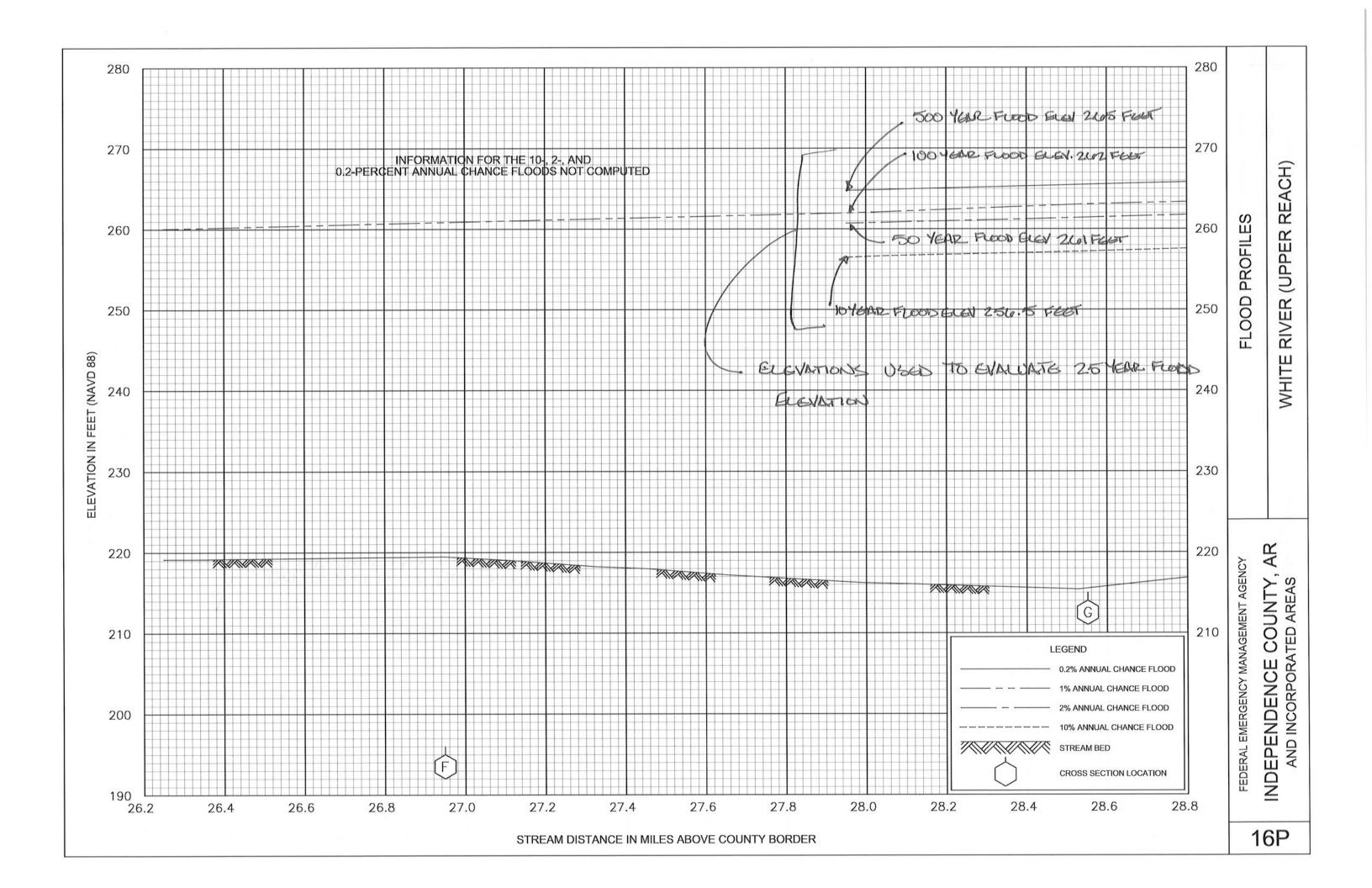


Federal Emergency Management Agency

FLOOD INSURANCE STUDY NUMBER 05063CV000B







Appendix B Storm Water Calculations

- Storm Water Run-On Estimate
- Pumping Time Estimate



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	0000 Cittles I in 211 Divin, Ontic 002, Di	non Rouge, En 10005 www		io.com	STILLT I OF 2
PROJECT / LOCATION	ON: Entergy Independence Steam Electric Stati		PROJECT / PROPOSAL NO.		
SUBJECT: Storm Wa	ater Capacity of West and East Recycle Ponds		302969.0000		
PREPARED BY: A. S	ampson	DATE: 9/5/2018	FINAL		
CHECKED BY: J. Ho	otstream	DATE: 9/9/2018	REVISION		

<u>Purpose</u>: Determine if 2 feet of freeboard is capable of containing the runoff volume from the 25-year, 24-hour storm event

Methodology:

- 1.) Determine the storage capacity of 2 feet Freeboard
- Storage Capacity of West Pond between EL. 235' and EL. 237'

S_{FB} Storage Volume at Freeboard (from attached HydroCAD model)

S_{TFB} Total Freeboard Storage Volume

 $S_{FB} = 587,616 \text{ ft}^3$

- Storage Capacity of East Pond between EL. 235' and EL. 237'

Freeboard Storage Capacity (Volumes are from attached HydroCAD model)

 $S_{FB} = 533,824 \text{ ft}^3$

-Total Freeboard Storage Capacity of West Pond and East Pond Combined

 $S_{TFB} = 1,121,440 \text{ ft}^3$

CTRC	8550 United Plaza Blvd, Suite 502, Baton Rouge, LA 70809 • www.TRCsolutions.com					
PROJECT / LOCAT	TION: Entergy Independence Steam Electr	ric Station - Newark, AR		PROJECT / PROPOSAL NO.		
SUBJECT: Storm Water Capacity of West and East Recycle Ponds				302969.0000		
PREPARED BY: A.	Sampson	DATE: 9/5/2018	FINAL			
CHECKED BY: 1. I	Hotstream	DATE: 9/9/2018	REVISION	П		

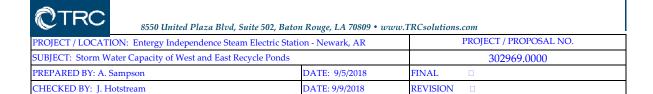
2.) Determine the storm water runon volume that flows into the basins from the 25-year, 24-hour storm event

$$V_R$$
 = Volume of Runon Area = 19.8 ac Rainfall Rate = 6.35 in/ac Design storm data from NOAA, refer to attached sheets V_R = Area * Rainfall Rate V_R = 456,400 ft³

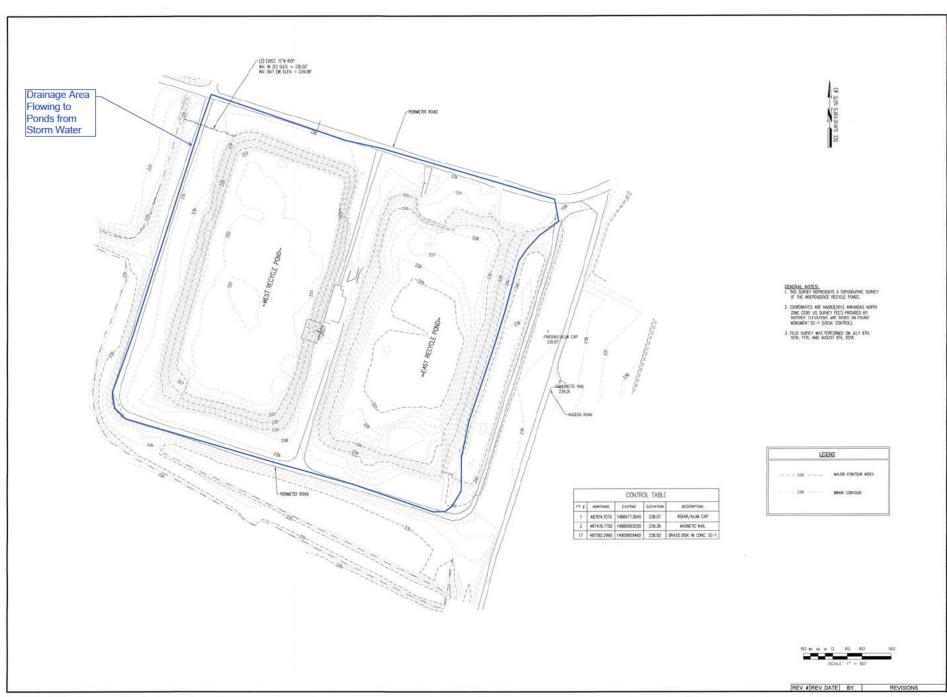
- 3.) Compare Freeboard Capacity to Volume of Runoff to dertmine if the Freeboard is capable of containing 100-year, 24-hour storm event.
- If $S_{TFB} > V_R$, then the Freeboard design is OK

$$S_{TFB} = 1,121,440 \text{ ft}^3$$
 $V_R = 456,400 \text{ ft}^3$
 $S_{FB} > V_R$

 $\underline{\underline{Conclusion}}: Because the S_{TFB} > V_R, the 2 feet of freeboard is capable of containing the runoff volume of the 25-year, 24-hour storm event$



ATTACHMENTS







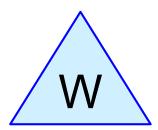
TOPOGRAPHIC SURVEY 555 POINT FERRY ROAD, NEWARK, AR INDEPENDENCE RECYCLE PONDS INDEPENDENCE COUNTY

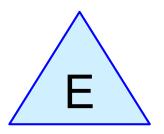
Design RLS 7/18 Checked Survey TAW 7/18
Fid.Bk.# 3177
Rev.#

BBF PROJ. 7-4183-0201 FILE NAME 001-FINAL SSUE DATE: 10/01/18

SCALE 1"=80"







West Pond

East Pond









Independence Recycle Ponds
Prepared by TRC
HydroCAD® 10.00-20 s/n 01402 © 2017 HydroCAD Software Solutions LLC

Printed 9/5/2018 Page 2

Area Listing (all nodes)

0.000	0	TOTAL AREA
(acres)		(subcatchment-numbers)
Area	CN	Description

Independence Recycle Ponds
Prepared by TRC
HydroCAD® 10.00-20 s/n 01402 © 2017 HydroCAD Software Solutions LLC

Printed 9/5/2018 Page 3

Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
0.000	HSG C	
0.000	HSG D	
0.000	Other	
0.000		TOTAL AREA

Independence Recycle Ponds
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Ground Covers (all nodes)

HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground	Subcatchment
(acres)	(acres)	(acres)	(acres)	(acres)	(acres)	Cover	Numbers
0.000	0.000	0.000	0.000	0.000	0.000	TOTAL	_
						AREA	

Independence Recycle Ponds

Prepared by TRC

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Rainfall not specified
Printed 9/5/2018
Page 5

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Pond E: East Pond Peak Elev=0.00' Storage=0 cf

Pond W: West Pond Peak Elev=0.00' Storage=0 cf

Rainfall not specified
Printed 9/5/2018
Page 6

Summary for Pond E: East Pond

[43] Hint: Has no inflow (Outflow=Zero)

volume	invert	Avaii.Sto	orage	Storage	Description		
#1	235.00'	834,6	22 cf	Custon	n Stage Data (Pr	ismatic)Listed below (Re	calc)
Elevation		.Area		Store	Cum.Store		
(feet) 235.00		sq-ft) 3,568	(cubi	c-feet)	(cubic-feet)		
236.00		4,923	25	59,246	259,246		
237.00		1,234		74,579	533,824		
238.00	317	7,361	30	00,798	834,622		

Rainfall not specified
Printed 9/5/2018
Page 7

Summary for Pond W: West Pond

[43] Hint: Has no inflow (Outflow=Zero)

Volume #1	Invert 235.00'	Avail.St 907,3	orage 352 cf		Description Stage Data (Pris	matic)Listed belo	ow (Recalc)
Elevation (feet)		sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)		
235.00 236.00		,201 ,688	28	0 39,945	0 289,945		
237.00 238.00		,655 ,817		97,672 19,736	587,616 907,352		



NOAA Atlas 14, Volume 9, Version 2 Location name: Newark, Arkansas, USA* Latitude: 35.6717°, Longitude: -91.4017° Elevation: 238.17 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS-	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹								ches)1	
Duration	Average recurrence interval (years)									
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.415 (0.355-0.489)	0.472 (0.403-0.556)	0.564 (0.481-0.665)	0.640 (0.544-0.756)	0.744 (0.620-0.889)	0.823 (0.677-0.990)	0.902 (0.728-1.10)	0.981 (0.773-1.21)	1.09 (0.836-1.35)	1.16 (0.884-1.46
10-min	0.608 (0.520-0.716)	0.691 (0.591-0.814)	0.826 (0.705-0.974)	0.937 (0.797-1.11)	1.09 (0.908-1.30)	1.21 (0.992-1.45)	1.32 (1.07-1.61)	1.44 (1.13-1.77)	1.59 (1.22-1.98)	1.70 (1.29-2.14)
15-min	0.741 (0.634-0.873)	0.842 (0.720-0.993)	1.01 (0.860-1.19)	1.14 (0.972-1.35)	1.33 (1.11-1.59)	1.47 (1.21-1.77)	1.61 (1.30-1.96)		1.94 (1.49-2.41)	
30-min	1.08 (0.922-1.27)	1.23 (1.05-1.44)	1.47 (1.25-1.73)	1.66 (1.41-1.97)	1.93 (1.61-2.31)	2.14 (1.76-2.57)	2.35 (1.89-2.85)	storm	ır, 24-ho event	ur 80
60-min	1.42 (1.21-1.67)	1.60 (1.37-1.89)	1.90 (1.62-2.24)	2.16 (1.83-2.55)	2.51 (2.10-3.01)	2.79 (2.30-3.36)	3.06 (2.48-3.73)	3.35 (2.65-4.13)	3.73 (2.88-4.66)	4.03 (3.06-5.06
2-hr	1.76 (1.52-2.05)	1.98 (1.71-2.31)	2.34 (2.02-2.73)	2.65 (2.27-3.10)	3.09 (2.61-3.67)	3.43 (2.86-4.10)	3.78 (3.09-4.58)	4.15 (3.31-5.08)	4.64 (3.62-5.76)	5.03 (3.86-6.27
3-hr	1.98 (1.72-2.29)	2.22 (1.92-2.57)	2.61 (2.26-3.04)	2.96 (2.55-3.44)	3.45 (2.93-4.09)	3.84 (3.22-4.58)	4.25 (3.49-5.12)	4.67 (3.75-5.70)	5.25 (4.12-6.49)	5.71 (4.41-7.09
6-hr	2.41 (2.11-2.76)	2.70 (2.36-3.10)	3.19 (2.78-3.66)	3.61 (3.14-4.16)	4.22 (3.62-4.96)	4.71 (3.99-5.56)	5.21 (4.33-6.23)	5.75 (4.66-6.96)	6.48 (5.14-7.95)	7.05 (5.50-8.70
12-hr	2.92 (2.58-3.32)	3.30 (2.91-3.75)	3.93 (3.46-4.47)	4.46 (3.92-5.09)	5.22 (4.52-6.07)	5.83 (4.97-6.81)	6.44 (5.40-7.63)	7.08 (5.80-8.50)	7.96 (6.37-9.69)	8.63 (6.80-10.6
24-hr	(3.49) (3.11-3.92)	(3.54-4.46)	4.76 (4.24-5.36)	5.42 (4.81-6.12)	6 35 (5.54-7.29)	7.07 (6.08-8.17)	7.79 (6.59-9.13)	8.54 (7.05-10.1)	9.53 (7.70-11.5)	(8.19-12.5
2-day	4.09 (3.69-4.55)	4.67 (4.20-5.19)	5.61 (5.04-6.24)	6.38 (5.72-7.13)	7.45 (6.56-8.46)	8.28 (7.19-9.47)	9.10 (7.76-10.6)	9.94 (8.28-11.7)	11.0 (9.00-13.2)	11.9 (9.55-14.3
3-day	4.49 (4.07-4.96)	5.11 (4.62-5.64)	6.11 (5.52-6.76)	6.94 (6.25-7.70)	8.08 (7.15-9.12)	8.96 (7.83-10.2)	9.85 (8.45-11.4)	10.7 (9.01-12.6)	11.9 (9.78-14.2)	12.8 (10.4-15.4
4-day	4.82 (4.38-5.30)	5.45 (4.96-6.00)	6.50 (5.90-7.16)	7.37 (6.66-8.14)	8.57 (7.61-9.63)	9.49 (8.33-10.8)	10.4 (8.98-12.0)	11.4 (9.58-13.3)	12.6 (10.4-15.0)	13.6 (11.0-16.3
7-day	5.61 (5.14-6.12)	6.30 (5.78-6.87)	7.45 (6.81-8.14)	8.41 (7.67-9.21)	9.74 (8.74-10.9)	10.8 (9.55-12.1)	11.8 (10.3-13.5)	12.9 (11.0-15.0)	14.4 (12.0-17.0)	15.5 (12.7-18.5
10-day	6.32 (5.83-6.85)	7.06 (6.50-7.66)	8.28 (7.61-9.00)	9.31 (8.53-10.1)	10.7 (9.69-11.9)	11.9 (10.6-13.3)	13.0 (11.4-14.8)	14.2 (12.1-16.4)	15.8 (13.2-18.6)	17.0 (14.0-20.2
20-day	8.43 (7.85-9.04)	9.30 (8.65-9.98)	10.7 (9.97-11.5)	11.9 (11.1-12.9)	13.6 (12.4-15.0)	14.9 (13.4-16.5)	16.2 (14.4-18.3)	17.6 (15.2-20.2)	19.4 (16.4-22.7)	20.8 (17.3-24.5
30-day	10.2 (9.57-10.9)	11.2 (10.5-12.0)	12.9 (12.1-13.8)	14.3 (13.3-15.3)	16.2 (14.8-17.7)	17.6 (16.0-19.4)	19.1 (17.0-21.4)	20.6 (17.9-23.4)	22.5 (19.1-26.1)	23.9 (20.1-28.1
45-day	12.5 (11.8-13.2)	13.8 (13.0-14.6)	15.8 (14.9-16.8)	17.5 (16.4-18.6)	19.7 (18.1-21.3)	21.4 (19.4-23.3)	23.0 (20.5-25.5)	24.5 (21.4-27.8)	26.6 (22.7-30.7)	28.0 (23.7-32.8
60-day	14.5 (13.7-15.2)	16.0 (15.1-16.9)	18.4 (17.4-19.4)	20.3 (19.1-21.5)	22.9 (21.1-24.5)	24.7 (22.5-26.8)	26.5 (23.7-29.2)	28.1 (24.6-31.7)	30.2 (25.9-34.7)	31.7 (26.9-37.0

Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

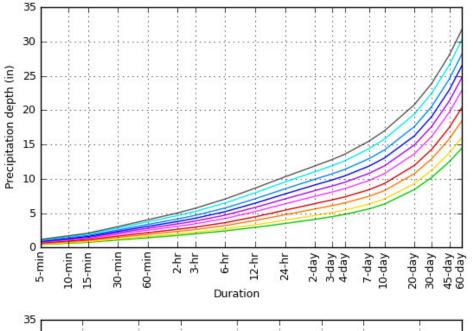
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

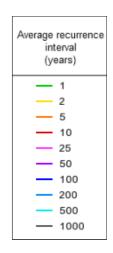
Please refer to NOAA Atlas 14 document for more information.

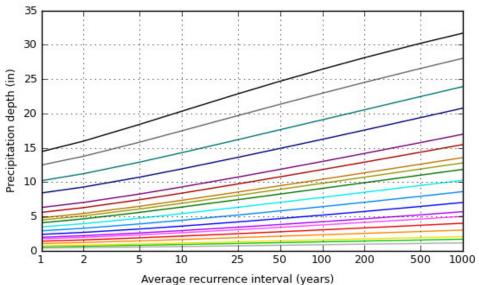
Back to Top

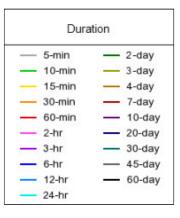
PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 35.6717°, Longitude: -91.4017°









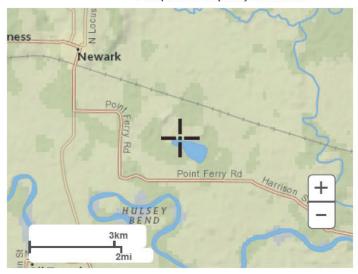
NOAA Atlas 14, Volume 9, Version 2

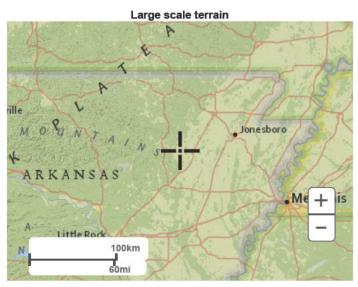
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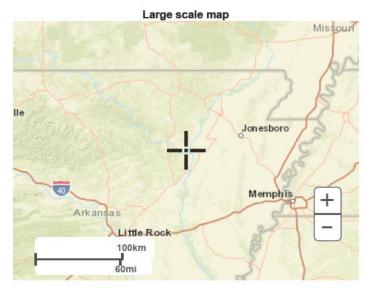
Back to Top

Maps & aerials

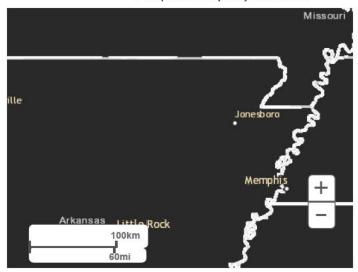
Small scale terrain







Large scale aerial



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Disclaimer



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SL	IFF.	Т1	OE

	0 -		
PROJECT / LOCATION: Entergy Independence Steam Electric Stati	PROJECT / PROPOSAL NO.		
SUBJECT: Estimated Pump Down Time	302969.0000		
PREPARED BY: J. Bell	DATE: 8/27/2018	FINAL	
CHECKED BY: J. Hotstream	DATE: 9/9/2018	REVISION	

<u>Purpose</u>: Determine the amount of time needed for the pump to remove the storm water collected during the 25-year, 24-hour storm event to design operation elevation (EL. 235)

Methodology:

1.) Use the volume of runon (V_R) from the Freeboard Volume Calculation (Refer to attached calculation sheet)

$$V_R = 456,400 \text{ ft}^3$$

- 2.) Use pump capacity rating to determine amount of time to lower the water level in both basins to EL. 235
- -Assume one pump is operational for each pond

$$\begin{array}{lll} \text{Pump Rate} &=& 2,750 & \text{gallons per minute (gpm)} \\ V_R &=& 3,414,109 & \text{gallons} \\ \\ \text{Time} &=& \frac{V_R}{(\text{Pump Rate})^*2} \\ \\ \text{Time} &=& 621 & \text{min} \\ &=& 10.3 & \text{hr} \\ &=& 0.4 & \text{days} \\ \end{array}$$

 $\underline{\textbf{Conclusion:}} \ \textbf{It will take approximately 10 hours to pump out the storm water to restablish freeboard after the 25-year, 24-hour storm event.}$